

LOCAL PARAMETERS OF THE SURFACE ROUGHNESS OF ELECTROCHEMICALLY DEALLOYED Ag-Pd ALLOYS

© 2018 E. V. Bedova, M. V. Grechkina, O. A. Kozaderov

Voronezh State University, 1, Universitetskaya pl., 394018 Voronezh, Russia
e-mail: ok@chem.vsu.ru

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Abstract. Local characteristics of surface roughness of the polycrystalline Ag-Pd solid solutions (4 and 8 at. % Pd) which underwent potentiostatic electrochemical dealloying in an acidic nitrate aqueous solution were determined by scanning electron and atomic force microscopy. A qualitative analysis of the SEM and AFM micrographs demonstrated substantial morphological roughening of the surface of Ag-Pd alloys. This results from the formation of hollows and cracks caused by selective leaching of electronegative silver and recrystallization of electropositive palladium into its highly-developed phase. A quantitative analysis of the AFM-data allowed us to determine the numerical values of the main local roughness characteristics of anodically modified alloys. The negative value of the coefficient of surface asymmetry indicates the formation of deep cavities during the dealloying process. The recorded mean roughness generally depends on the AFM-scanning zone, but it stabilizes if the scan zone exceeds several tens of micrometers. The roughness of dealloyed Ag-Pd systems is of micro- and nano-size and increases with anodic potential and electric charge of the electrochemical modification of both studied Ag₄Pd and Ag₈Pd alloys. This effect can be accounted for by a significant rise in the anodic dissolution rate of silver from the alloys in the overcritical region of polarization, resulting in the formation of deeper surface defects. An increase in the average height of surface irregularities with modification time conforms to the square root law, confirming the non-stationary mass transfer kinetics of the selective dissolution process. Variation of the anodic potential and electric charge makes it possible to find the optimal conditions for the electrochemical synthesis of electrode Ag-Pd materials with given values of arithmetic mean and root-mean-square roughness. The assumption that harmonic sinusoidal function represents the Ag-Pd surface microprofile proved the linear dependence of the roughness factor on dealloying time.

Keywords: dealloying, Ag-Pd alloys, surface roughening, SEM, AFM.

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INTRODUCTION

Anodic dissolution and corrosion of alloys often becomes selective [1–3] due to significant difference of components in thermodynamic and electrochemical properties. Selective dissolution (SD) leads to the formation of a non-equilibrium surface layer, whose chemical, phase and microstructural state is changed compared with the bulk of the alloy [4]. Especially significant changes can be appeared if *A-B* alloy undergoes anodic dissolution in the overcritical region of potentials and charges, when, along with ionization of electronegative component *A*, recrystallization of noble metal *B* into its own nanoporous or dispersed phase takes place [5–11]. As a consequence, the dealloying process can be used to synthesize electrode materials characterized

by a morphologically highly developed surface. Indeed, the corrosive etching of the active metal in a chemically aggressive solution makes it possible to obtain fine powders and monolithic spongy metals, for example, gold [5, 7, 10], silver [7], and palladium [6, 7, 11].

The disadvantage of free corrosion dealloying is the uncontrolled pore size of the synthesized material. On the contrary, using electrochemical anodic SD it is possible to regulate the morphological properties and chemical composition of the surface layer of a dealloyed material [8–10], and to obtain nanoporous materials with a highly developed surface structure. Moreover, deep electrochemical etching allows to synthesize materials that do not require additional stabilization in a matrix [10, 11].

The highly developed surface layer forming at SD of an alloy is characterized by an increased area of the electrode / electrolyte interface. The problem of determining the local and integral morphological parameters of the surface of anodically modified alloys is actual both in the kinetic description of the electrochemical processes occurring on it, and in substantiating the possibility of practical use of materials synthesized by the method of selective dissolution.

There are two measures of the surface area of a real solid electrode [12], namely the true surface area (S_{real}) and geometric one (S_{geom}); their ratio is equal to the roughness factor f_r [13]:

$$f_r = S_{\text{real}}/S_{\text{geom}} \quad (1)$$

Unfortunately, there is no universal method for determining S_{real} and f_r , because their values depend on the measurement method, on the theoretical model on which this method is based, and on the conditions of its application [14]. In addition, S_{real} and f_r are the integral parameters of the electrode surface and do not allow describing the local geometric characteristics of the surface. To determine the latter, scanning electron microscopy (SEM) and atomic force microscopy (AFM) methods are used. The arithmetic average roughness R_a , the mean square roughness R_q and the radial wavelength L_a make it possible to sufficiently characterize the microrelief of the surface of an alloy subjected to SD. The parameter R_a is defined as the average deviation of all points of the AFM image from the mid-plane, and R_q – as the average value of the measured deviations from the mid-plane. The quantity L_a serves as a parameter of the periodicity of the surface structure and, in fact, is the average distance between adjacent irregularities [15].

The purpose of this work is the microscopic determination of the local characteristics of a highly developed surface of Ag-Pd alloys formed by anodic selective dissolution in an acidic nitrate aqueous solution in the overcritical region of anodic potentials and electric charges.

EXPERIMENTAL

Polycrystalline homogeneous alloys of the Ag-Pd system with bulk atomic fraction of palladium 4 and 8 at. % obtained by direct alloying of the components according to the procedure described in [16], were selected for the study. Making electrodes, the alloys were cut, polished, and placed in a frame of polymerized epoxy resin. Preparation of the working surface of the electrodes included stripping on sanding paper, polishing on chamois with an aqueous MgO suspen-

sion to a mirror finish, degreasing with ethyl alcohol, and washing twice with bidistilled water.

Anodic selective dissolution of Ag-Pd alloys was carried out at room temperature in an unmixed and de-aerated with argon solution of 0.1 M KNO_3 + 0.001 M HNO_3 + 0.001 M AgNO_3 under potentiostatic polarization conditions using the IPC-Pro-L electrochemical complex in a standard three-electrode cell with non-separated cathode and anode spaces. The auxiliary electrode was Pt. The silver chloride reference electrode was located in a separate vessel and connected to the cell by an electrolytic bridge filled with a saturated solution of ammonium nitrate, with a Luggin capillary. The solution was prepared on bidistilled water using salts of reagent and analytical grade, as well as a pre-standardized solution of acid. The potentials E are given relative to the standard hydrogen electrode scale, the specific charge q is calculated per unit of the true initial surface area of the Ag-Pd electrode, the roughness factor of which is determined by a combined electrochemical method [17].

The critical potentials and charges corresponding to the start of the surface development of the systems under study, evaluated by the chronoamperometry method according to [18], are listed in the table.

Table. The critical potential E_{cr} and critical charge q_{cr} of selective dissolution of Ag-Pd alloys in 0.1 M KNO_3 + 0.001 M HNO_3 + 0.001 M AgNO_3

Alloy	E_{cr} , mV	q_{cr} , mC/cm ²
Ag4Pd	703	0.5
Ag8Pd	717	0.8

The morphological development of the surface layer of the Ag4Pd alloy was carried out at a constant overcritical potential $E_{\text{mod}} > E_{\text{cr}}$. The Ag8Pd alloy was subjected to anodic modification with variable values of both electric charge $q_{\text{mod}} > q_{\text{cr}}$ and electrode potential $E_{\text{mod}} > E_{\text{cr}}$.

Local data on the surface microrelief of Ag-Pd electrodes were obtained on JSM-6510LV electron microscope (JEOL Ltd) and on Solver P47PRO atomic force microscope (NSG 20 cantilever, made of silicon and coated with gold) in a semicontact (intermittent-contact) scanning mode of a sample. The surface study of the samples was carried out at five different points of a scanning area of mesoscopic ($65 \times 65 \mu\text{m}^2$, $10 \times 10 \mu\text{m}^2$) and microscopic ($2 \times 2 \mu\text{m}^2$, $1 \times 1 \mu\text{m}^2$) size. The local parameters of the surface microrelief were found from the data of digital and statistical processing of the obtained AFM images in the Gwyddion

2.30 soft. The results of the SEM and AFM studies were obtained in the Voronezh State University Center for collective use of scientific equipment (CKPNO VGU).

RESULTS AND DISCUSSION

Micrographs of the surface of the samples obtained by the SEM method confirm the substantial morphological development of the surface layer of Ag-Pd alloys after their overcritical selective dissolution (Fig. 1). Figures 2 and 3 show the AFM images and surface microprofiles of the studied Ag-Pd alloys. Along with the texture caused by the preparation of the samples for the experiment, there are additional cavities formed directly during the process of electrochemical dissolution of silver from the Ag-Pd alloy.

The advantage of the AFM method in comparison with scanning electron microscopy is the ability to determine the numerical values of the local roughness characteristics of anodically modified alloys. For instance, the analysis

showed that the coefficient of asymmetry, which characterizes the skewness of the distribution of the microprofile [15], takes mostly negative values. This indicates that not protrusions predominate on the surface of the anodically modified alloy, but hollows formed, apparently, during the selective dissolution of silver and recrystallization of palladium.

It turned out that the microscopically detected root-mean-square roughness R_q increases with the size of the scanning zone (L_{xy}) if $R_q > L_{xy}$. However, under the condition $L_{xy} > 50 \mu\text{m}$, this parameter reaches an almost constant value (Fig. 4). This is consistent with the literature data on the ambiguity of the results of determining morphological characteristics by microscopic methods, if the characteristic length of the scan area does not exceed the average size of the irregularities of the surface under study [15, 19, 20].

At the same time, regardless of the value of L_{xy} , an increase in nanometer roughness with an increase in the value of charge q_{mod} is observed

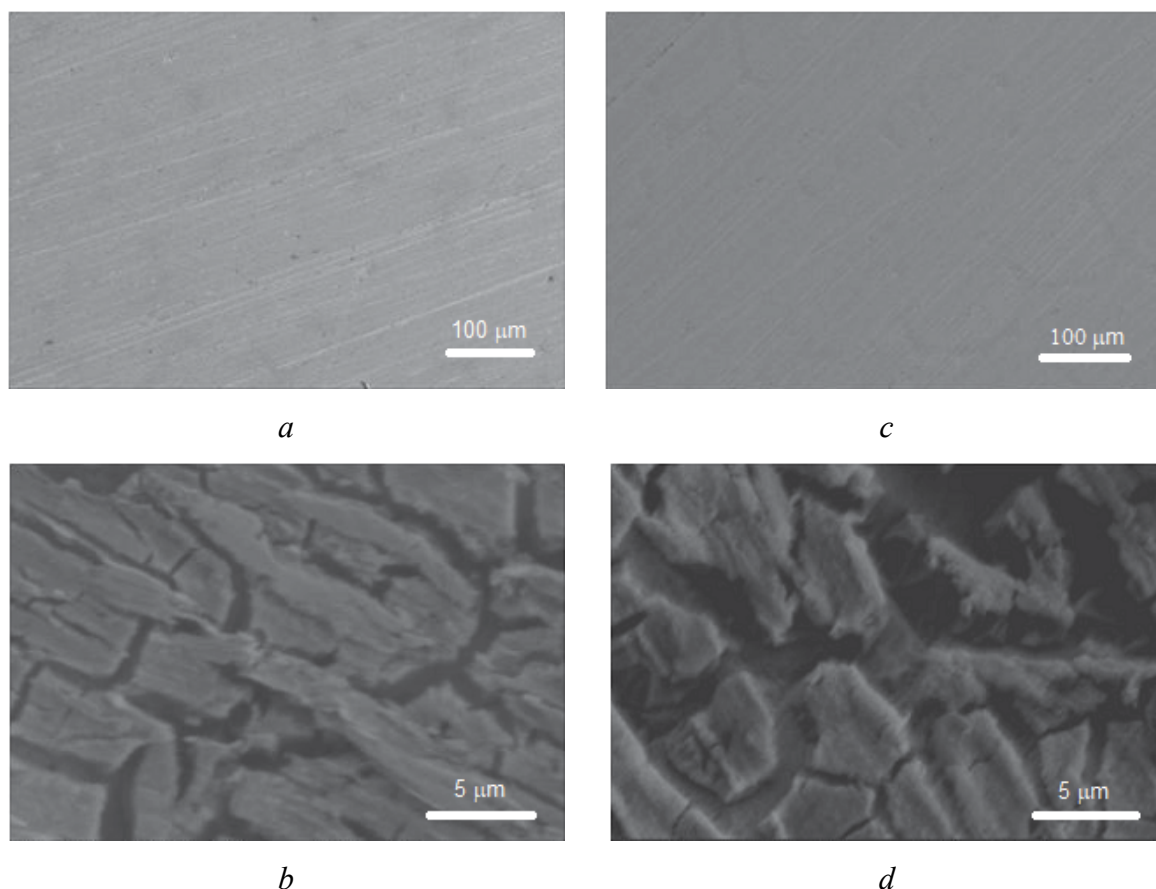


Fig. 1. SEM images of the surface of Ag4Pd (*a, b*) and Ag8Pd alloys (*c, d*) in the initial state (*a, c*) and after anodic modification (*b, d*). Modification mode: solution 0.1 M KNO_3 + 0.001 M HNO_3 + 0.001 M AgNO_3 , modification potential $E_{\text{mod}} = E_{\text{cr}} + 185 \text{ mV}$, charge $q_{\text{mod}} \cong 500q_{\text{cr}}$

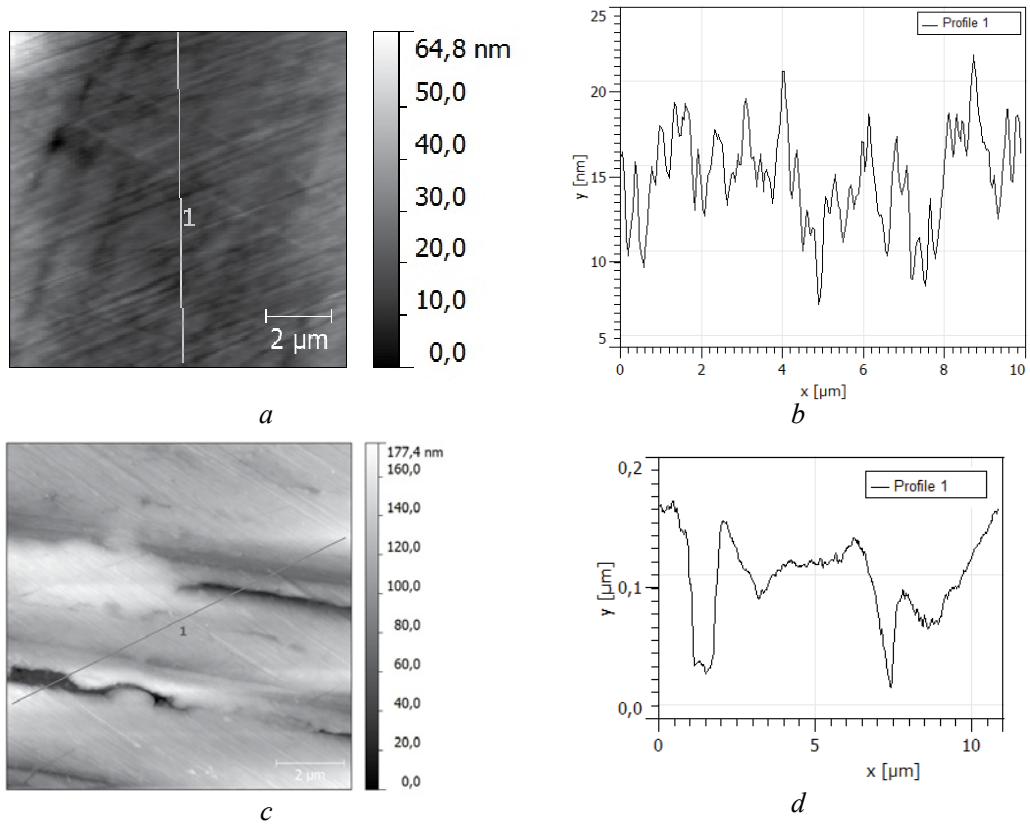


Fig. 2. Topographic AFM images and microscopic profiles of the surfaces of anodically modified Ag4Pd alloy in the initial state (*a, b*) and after anodic modification (*c, d*). Modification mode: $E_{\text{mod}} = 888 \text{ mV}$, $q_{\text{mod}} = 141 \text{ mC/cm}^2$

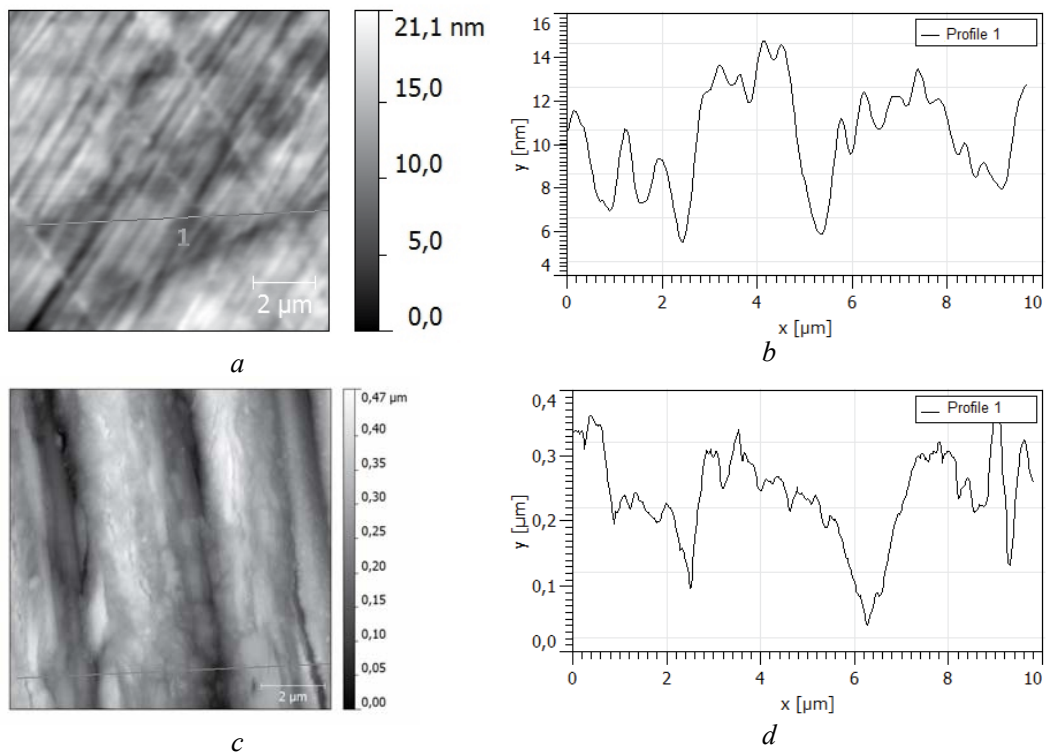


Fig. 3. Topographic AFM images and microscopic profiles of the surfaces of anodically modified Ag8Pd alloy in the initial state (*a, b*) and after anodic modification (*c, d*). Modification mode: $E_{\text{mod}} = 903 \text{ mV}$, $q_{\text{mod}} = 243 \text{ mC/cm}^2$

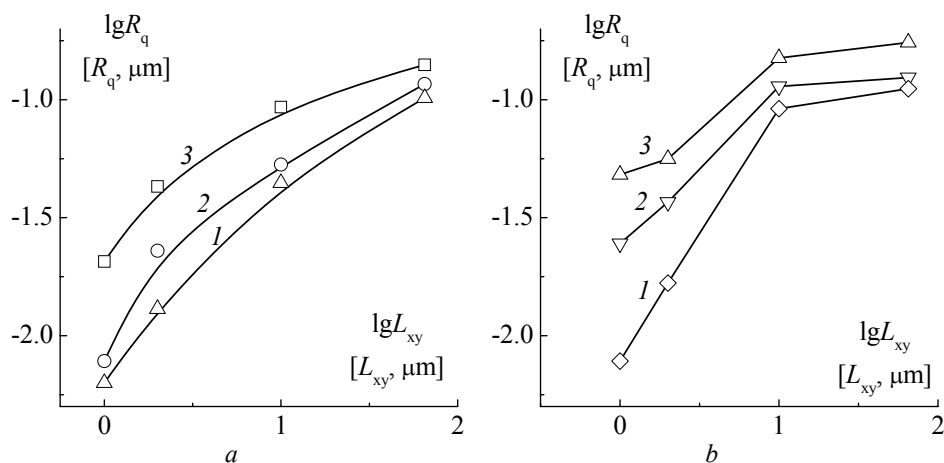


Fig. 4. Root-mean-square roughness vs. scan area size curves for anodically modified alloys Ag4Pd (a) and Ag8Pd (b). Modification modes: (1) - $E_{\text{mod}} = 888$ mV, $q_{\text{mod}} = 28$ mC/cm², (2) - $E_{\text{mod}} = 888$ mV, $q_{\text{mod}} = 56$ mC/cm², (3) - $E_{\text{mod}} = 888$ mV, $q_{\text{mod}} = 113$ mC/cm², (4) - $E_{\text{mod}} = 773$ mV, $q_{\text{mod}} = 16$ mC/cm², (5) - $E_{\text{mod}} = 823$ mV, $q_{\text{mod}} = 58$ mC/cm², (6) - $E_{\text{mod}} = 903$ mV, $q_{\text{mod}} = 486$ mC/cm²

for both Ag4Pd and Ag8Pd alloys (Fig. 5). Using the example of Ag8Pd system, it was also found that the parameters R_a and R_q increase with increasing excess of the potential E_{mod} of the anodic modification over the critical value E_{cr} . The observed effect can be explained by a noticeable increase in the rate of the dealloying process at $E > E_{\text{cr}}$, $q > q_{\text{cr}}$ [1, 2, 4] and, as a result, by the formation of deeper extended structural defects in the surface layer of selectively dissolving Ag-Pd alloys.

Thus, varying the values of anode potential E_{mod} and charge q_{mod} passed through the system allows to obtain electrode materials with a given degree of surface development, manifested in the appearance of channels and cracks of nano- and micrometer scale, which are absent before the onset of anodic polarization.

Along with the arithmetic mean and root-mean-square roughness, we determined the radial wavelength of the microrelief L_a , and estimated the dependence of the surface development factor on time $f_r(t)$. We used the simplifying assumption that the microprofile of the surface of Ag-Pd electrodes can be described by a harmonic sinusoidal function. It was taken into account that if the roughness values R_a are significantly less than the average distance between the irregularities L_a , then the following expression can be used the dependence of the roughness factor on the time of anodic selective dissolution of the alloy [21]:

$$f_r(t) \approx 1 + \frac{2\pi^2 \cdot R_a^2(t)}{L_a^2}. \quad (2)$$

The analysis showed that the average height of surface irregularities increases with time of anodic modification according to the square root law (Fig. 6), i.e. $R_a(t) \approx \text{const} \cdot \sqrt{t}$. This indirectly confirms the data on the diffusion control of the process of selective dissolution of Ag-Pd alloys in an acidic nitrate medium, previously obtained by non-stationary electrochemical methods [16]. Moreover, the average wavelength L_a of a microprofile takes a constant value, and $L_a \gg R_a$. Taking into account the totality of the analysis data, the dependence of the surface development degree on time can be described by a linear function as follows:

$$f_r(t) \approx 1 + \text{const} \cdot t. \quad (3)$$

This function coincides with the formula for the transient roughness factor of selectively dissolving studied Ag-Pd-alloys which we obtained earlier [22] using the voltammetric method. This indicates a correlation between the integral and local characteristics of the surface roughness of the studied electrode systems, which were found independently using non-stationary electrochemical and microscopic methods.

CONCLUSION

The surface roughening of Ag-Pd alloys during dealloying in nitrate aqueous solution is confirmed by SEM and AFM methods. It was shown that the local roughness of anodically modified alloys increas-

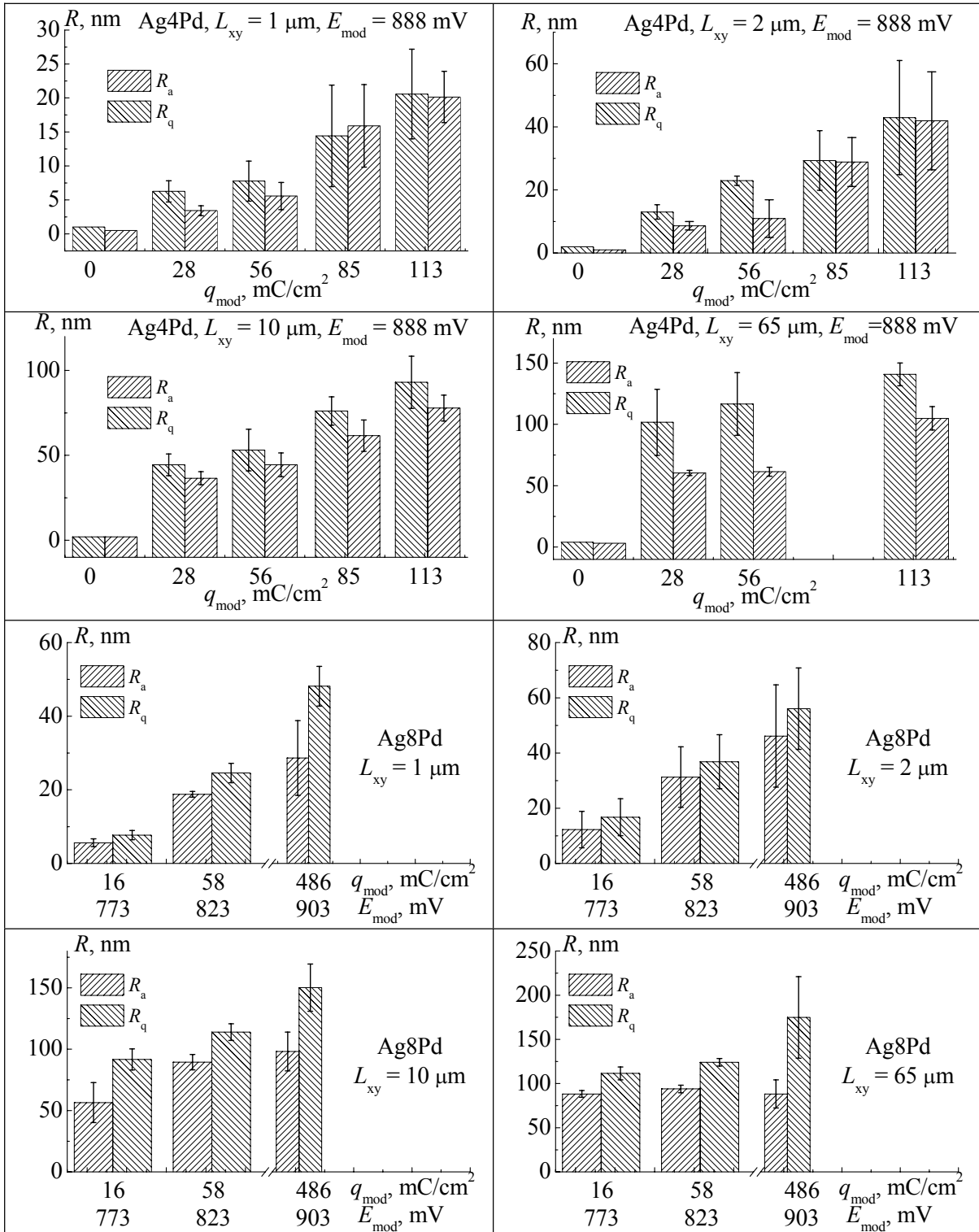
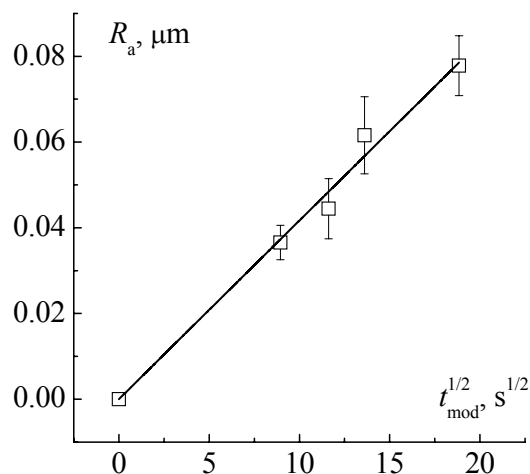


Fig. 5. Average surface roughness of Ag-Pd alloys at different conditions of anodic modification. L_{xy} is a AFM scanning area size

es with the overcritical potential and charge of anodic dissolution for both studied Ag₄Pd and Ag₈Pd alloys. Using the results of the work it is possible to optimize the conditions of the electrochemical dealloying synthesis of new electrode materials with given integral and local characteristics of the surface, such as the real surface area, arithmetic mean and root-mean-square roughness, as well as radial wavelength of the microrelief.

Fig. 6. Criterion dependence of the arithmetic mean surface roughness of Ag₄Pd alloy on time of anodic modification, $E_{\text{mod}} = 888$ mV



УДК 544.653.22+539.211

ЛОКАЛЬНЫЕ ПАРАМЕТРЫ ШЕРОХОВАТОСТИ ПОВЕРХНОСТИ АНОДНО-МОДИФИЦИРОВАННЫХ Ag,Pd-СПЛАВОВ

© 2018 Е. В. Бедова, М. В. Гречкина, О. А. Козадеров

Воронежский государственный университет, Университетская пл., 1, 394018 Воронеж, Россия
e-mail: ok@chem.vsu.ru

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Аннотация. Локальные характеристики шероховатости поверхности поликристаллических твердых растворов системы Ag-Pd (4 и 8 ат.% Pd) после их потенциостатического электрохимического селективного растворения в кислой нитратной водной среде определены с помощью сканирующей электронной и атомно-силовой микроскопии. Качественный анализ СЭМ- и АСМ-микрофотографий подтверждает существенное морфологическое развитие поверхности Ag,Pd-сплавов из-за образования пор и трещин, вызванного избирательным вытравливанием электроотрицательного компонента (серебра) и перекристаллизацией электроположительного компонента (палладия) в собственную высокоразвитую фазу. Количественным анализом АСМ-данных определены численные значения основных характеристик локальной шероховатости анодно-модифицированных сплавов. Отрицательное значение коэффициента поверхностной асимметрии указывает на образование глубоких полостей во время процесса селективного растворения. Средняя микро- и нанощероховатость поверхности сплавов Ag₄Pd и Ag₈Pd не зависит от размера зоны АСМ-сканирования, если он превышает несколько десятков микрометров, а также увеличивается с анодным потенциалом и электрическим зарядом электрохимической модификации. Данный эффект можно объяснить существенным повышением скорости анодного растворения серебра из сплавов в закритической области анодной поляризации, что приводит к образованию более глубоких поверхностных дефектов. Увеличение средней высоты неровностей поверхности со временем модификации подчиняется закону квадратного корня, что косвенно подтверждает нестационарную диффузионную кинетику процесса селективного растворения. Варьирование анодного потенциала и электрического заряда позволяет оптимизировать условия электрохимического синтеза электродных Ag,Pd-материалов с заданными значениями среднеарифметической и среднеквадратичной шероховатости. В предположении, что микропрофиль поверхности Ag,Pd-сплавов описывается гармонической синусоидальной функцией, подтверждена линейная зависимость фактора шероховатости от времени селективного растворения.

Ключевые слова: селективное растворение, Ag,Pd-сплавы, шероховатость поверхности, СЭМ, АСМ.

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Бедова Евгения Валерьевна – аспирант кафедры физической химии, Воронежский государственный университет, Воронеж, Россия; тел.: +7(473) 2208538; e-mail: iev.vsu@mail.ru

Гречкина Маргарита Владимировна – ведущий инженер кафедры физики полупроводников и микроэлектроники, Воронежский государственный университет, Воронеж, Россия; тел.: +7(473) 2208481, e-mail: grechkina_m@mail.ru

Козадеров Олег Александрович – д. х. н., доцент кафедры физической химии, Воронежский государственный университет, Воронеж, Россия; тел.: +7(473) 2208538; e-mail: ok@chem.vsu.ru

Eugenia V. Bedova – postgraduate, Physical Chemistry Department, Voronezh State University, Voronezh, Russia; tel.: +7(473) 2208538, e-mail: iev.vsu@mail.ru

Margarita V. Grechkina – Leading Engineer, Semiconductor Physics and Microelectronics Department, Voronezh State University, Voronezh, Russia; tel.: +7(473) 2208481, e-mail: grechkina_m@mail.ru

Oleg A. Kozaderov – Dr. Sci. (Chem.), Associate Professor, Physical Chemistry Department, Voronezh State University, Voronezh, Russia; tel.: +7(473) 2208538; e-mail: ok@chem.vsu.ru